

# Mclean seminar

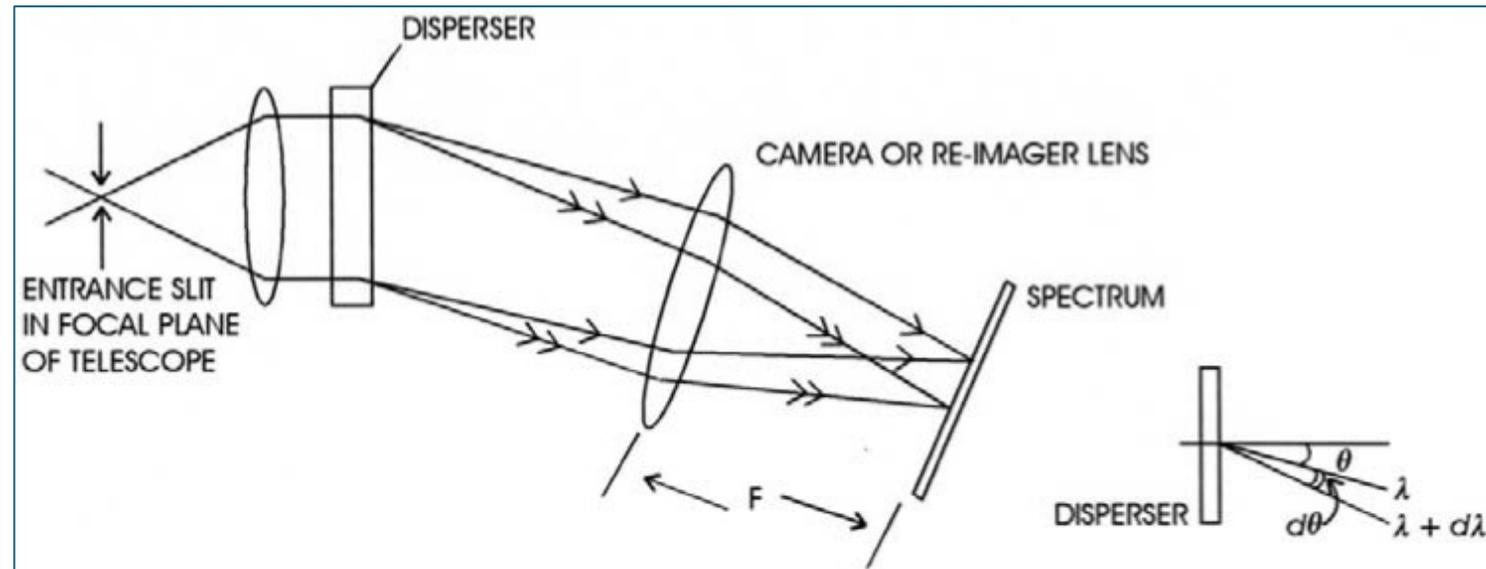
## sec.5.2-5.2.4

2024/06/28

M1 Kensho Tanaka

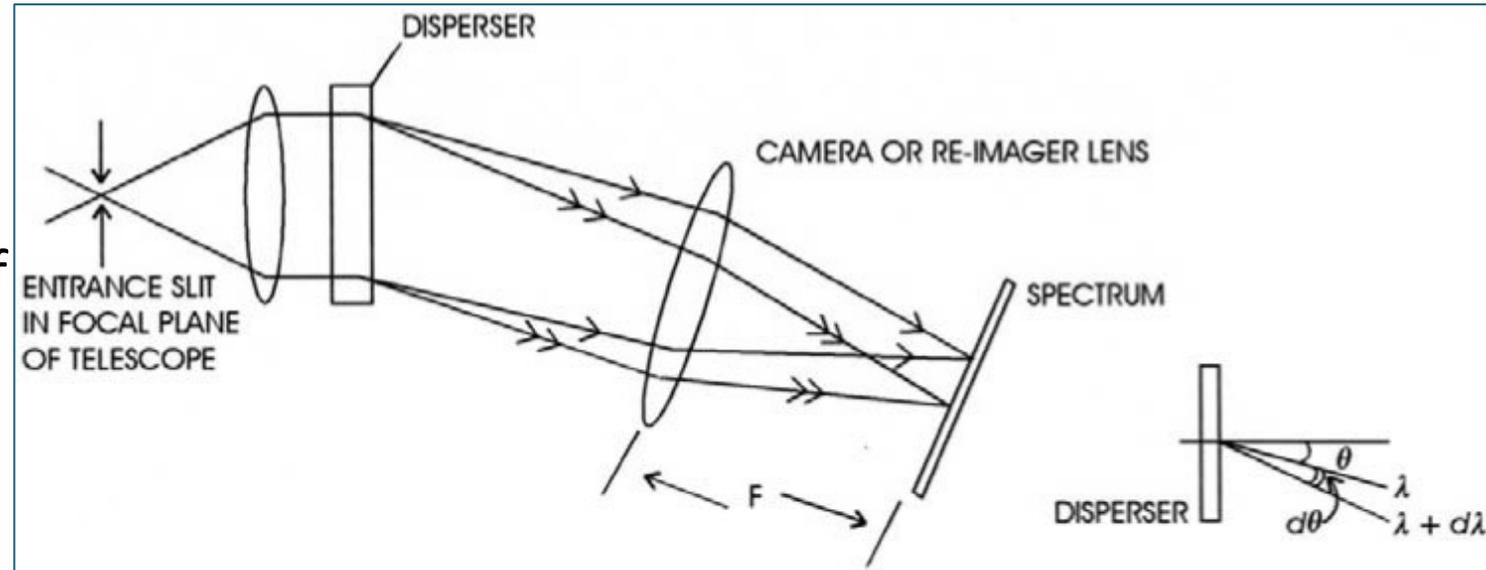
# 5.2 Spectrometers

- All spectrometers have essentially the same basic design.
- But many different implementations are possible depending on the constraints and choice of **spectral disperser**.



# 5.2 Spectrometers

- The important quantities
  - the resolving power ( $R$ )
  - the slit width
  - the diameter of the collimated beam
  - the sampling or matching of the slit width to the detector pixels
  - the resulting  $f$ /number of the camera system



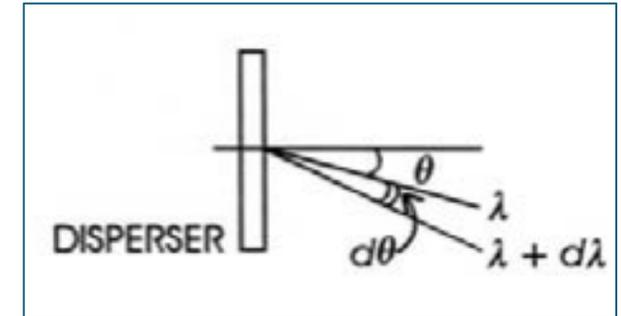
# 5.2.1 Resolution and dispersion

- Angular Dispersion (AD)
  - the rate of change of the dispersed angle of the beam with respect to wavelength

$$AD = \frac{d\theta}{d\lambda}$$

- Linear Dispersion (LD)
  - relates an interval of length ( $dx$  in millimeters) along the spectrum to a wavelength interval (mm/A)

$$LD = \frac{dx}{d\lambda} = \frac{dx}{d\theta} \frac{d\theta}{d\lambda} = f_{cam} AD$$



# 5.2.1 Resolution and dispersion

- Resolving Power

- the ability to distinguish two wavelengths separated by a small amount  $\Delta\lambda = \lambda_2 - \lambda_1$

$$R = \frac{\lambda}{\Delta\lambda}$$

- Resolution is often stated

$$\frac{1}{R} = \frac{\Delta\lambda}{\lambda} = \frac{V}{c}$$

- where the non-relativistic Doppler formula
- (e.g.  $R = 10000 > V = 0.0001c = 30\text{km/s}$ )

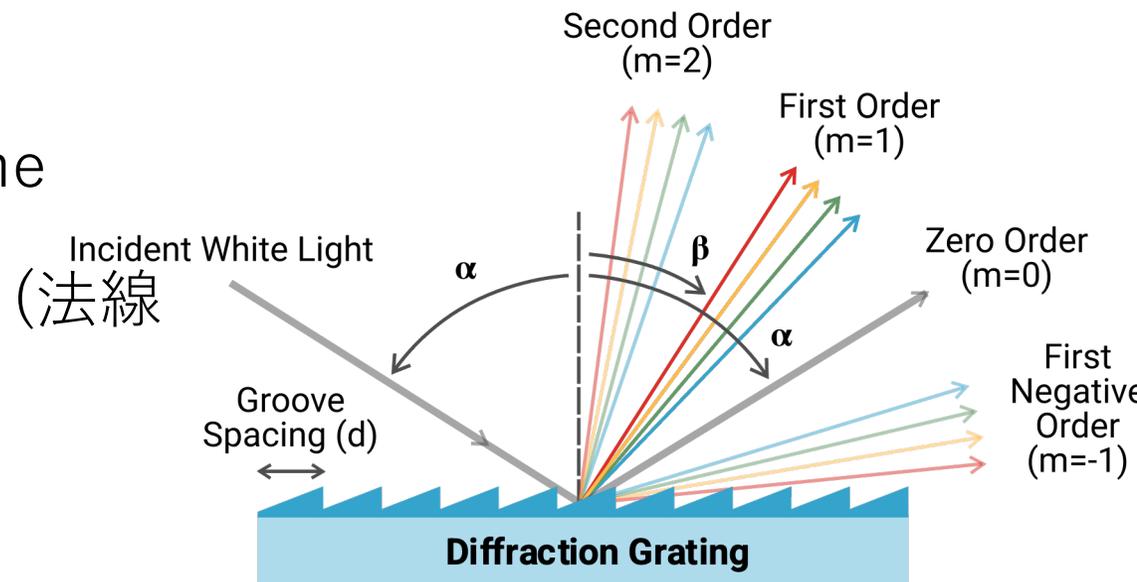
# 5.2.2 Diffraction gratings

- The usual dispersing element is a diffraction grating and the general grating equation is

$$m\lambda = d(\sin i + \sin \theta) \cos \gamma$$

- $d$  : the spacing of adjacent grooves or slits
  - $i$  (represented by  $\alpha$ ) : the angle of incidence of the collimated beam
  - $\theta$  (represented by  $\beta$ ) : the angle of the emergent diffracted beam
  - $\gamma$  : the angle out of the normal plane (法線平面) of incidence (usually  $0^\circ$ )
  - $m$  : an integer called the “order” of interference
- It can apply when the grating is used in transmission or in reflection

Grating and Diffraction Orders



(<https://www.meetoptics.com/academy/grating-density>)

# 5.2.2 Diffraction gratings

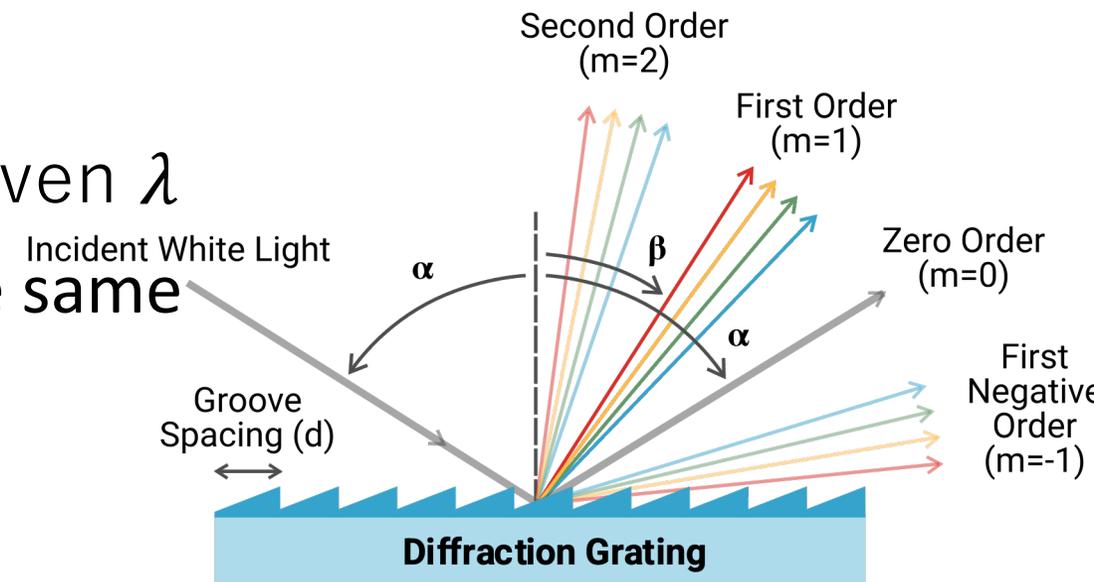
- The alternative form

$$m\lambda = d(\sin i + \sin \theta) \cos \gamma$$

$$AD = \frac{d\theta}{d\lambda} = \frac{m}{d \cos \theta \cos \gamma} = \frac{\sin i + \sin \theta}{\lambda \cos \theta}$$

- AD is determined by  $i$  and  $\theta$  for a given  $\lambda$
- Many combinations of  $m$  and  $d$  yield the same AD provided the grating angles remain unchanged

Grating and Diffraction Orders



(<https://www.meetoptics.com/academy/groove-density>)

## 5.2.2 Diffraction gratings

- Typical “first-order gratings” ( $m \sim 1$ ) have 300-2,400 grooves or lines/millimeter.
- the number of lines per millimeter is given by  $T = 1/d$ .
- $\cos\theta \sim 1$  and slowly varying
  - AD is almost constant
  - the relationship between position and wavelength on the detector (Equation (5.8), the upper equation) is approximately linear.

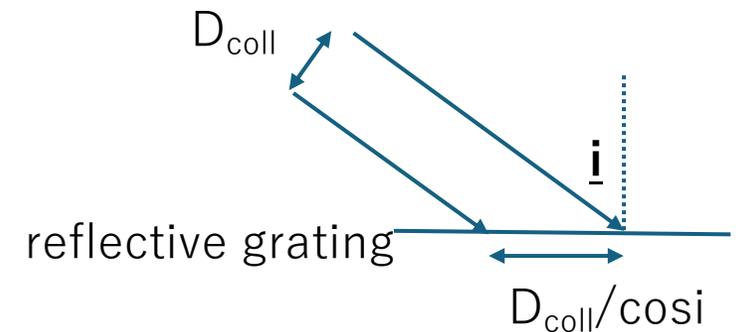
$$LD = \frac{dx}{d\lambda} = \frac{dx}{d\theta} \frac{d\theta}{d\lambda} = f_{cam} AD$$
$$AD = \frac{d\theta}{d\lambda} = \frac{m}{d \cos \theta \cos \gamma} = \frac{\sin i + \sin \theta}{\lambda \cos \theta}$$

## 5.2.2 Diffraction gratings

- “Echelle” gratings
  - Coarse-ruled reflection gratings (**large  $d$ , small  $T$** ) can achieve high angular dispersion by making  $i$  and  $\theta$  very large.
  - groove densities :  $T = 20\text{-}200$  lines/millimeter
  - $m : 10\text{-}100$
  - this results in severe overlap of orders unless a second disperser of lower resolving power at right angles to the first is used to “separate” the orders.

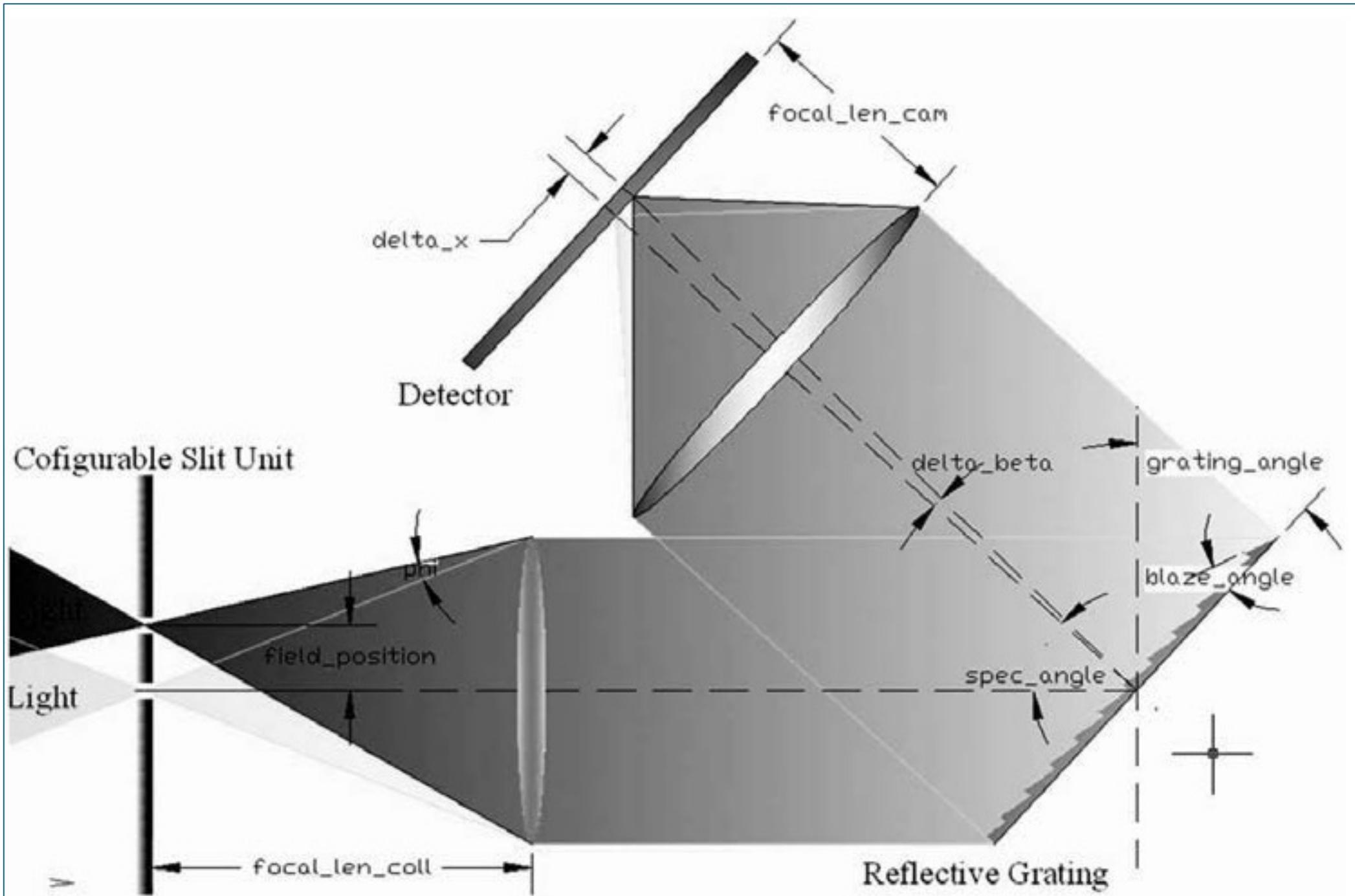
## 5.2.2 Diffraction gratings

- In a standard astronomical spectrograph, the light emerging from the slit
  - is collimated into the parallel beam of diameter  $D_{\text{coll}}$
  - directed onto a reflection grating at an angle of incidence  $i$
  - so that illuminated length is  $D_{\text{coll}} / \cos i$
- The magnification between the slit and the detector :  
 $f_{\text{cam}} / f_{\text{coll}}$



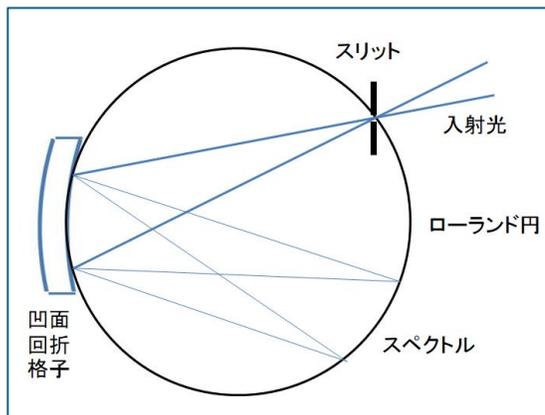
## 5.2.2 Diffraction gratings

- It is much more convenient
  - to keep **the collimator** and **the camera optics** in a **fixed** position
  - to **allow** some limited motion of **gratings**
    - than to **fix the grating** and require **the camera optics to move in an arc** (弧状に動かす) to pick up different parts of the diffracted beam.
- Two optical axes
  - defined by collimator
  - defined by the camera
  - These axes intersect on the reflection grating.

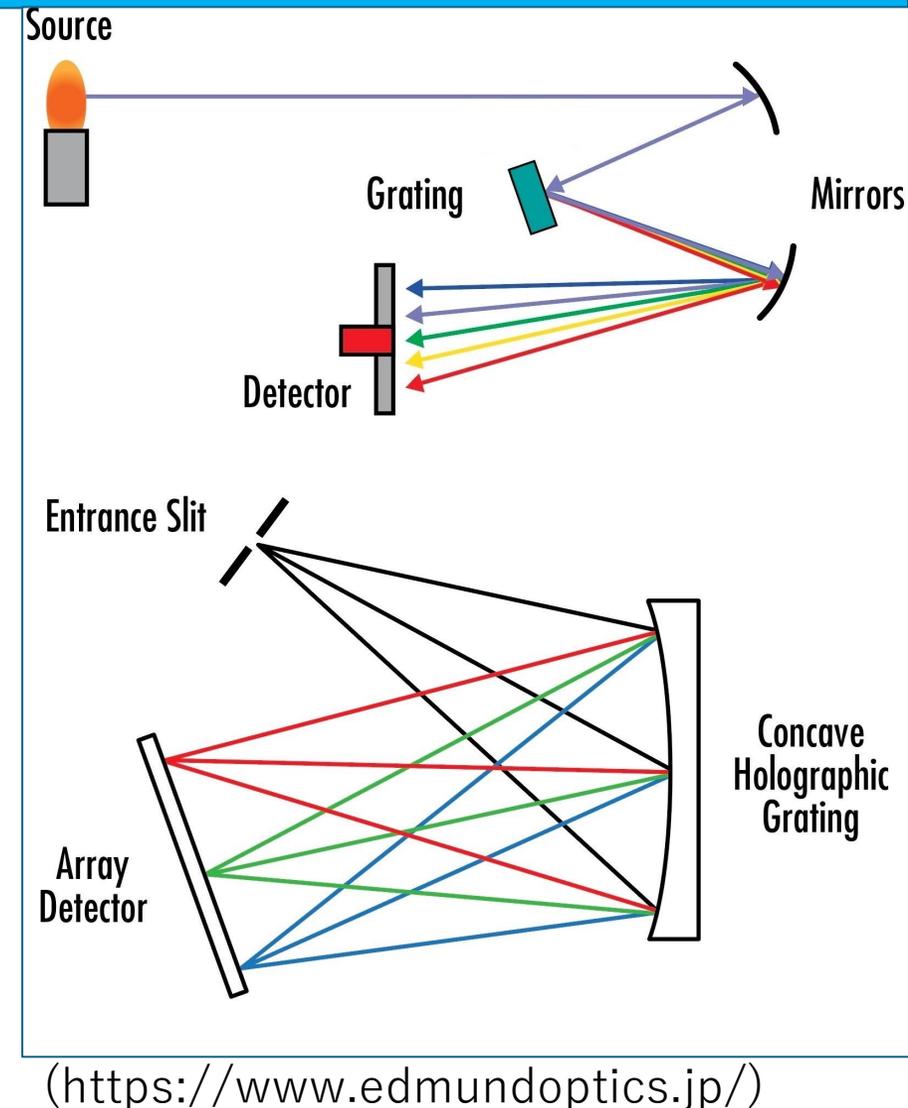


# 5.2.2 Diffraction gratings

- The example of concave gratings (lower picture)
  - this approach is ideally suited for the **far-ultraviolet** where transmission lenses are difficult to obtain.
- Rowland Circle
  - the circle which has the same curvature of concave grating



(<https://astro-dic.jp/rowland-circle/>)



(<https://www.edmundoptics.jp/>)

## 5.2.2 Diffraction gratings

- A grating produces a different magnification in the dispersion direction than at right angles to the dispersion.
- The “anamorphic” magnification factor describes this effect and is found by determining the change in  $\theta$  for a change in  $i$

$$\frac{d\theta}{di} = \left| \frac{\cos i}{\cos \theta} \right|$$

- the size of the slit image ( $\Delta x$ ) at the detector becomes

$$\Delta x = w \frac{\cos i}{\cos \theta} \frac{f_{cam}}{f_{coll}}$$

- $w$  : slit width



## 5.2.2 Diffraction gratings

- If the grating is to accept all the light from the collimator then it follows that the ruled width of the grating ( $W$ )

$$W = D_{coll} / \cos i$$

- In the diffraction-limited case

$$R = mN = \frac{mW}{d} = \frac{W(\sin i + \sin \theta)}{\lambda}$$

- $N$  : the total number of grooves illuminated
- In practice, spectrometers are usually slit width limited or seeing-limited.

## 5.2.2 Diffraction gratings

- In practice, spectrometers are usually slit width limited or seeing-limited.

- If the slit width  $\sim$  seeing disk,  $\theta_{see} = \lambda/D_{tel}$

$$R = \frac{W(\sin i + \sin \theta)}{\theta_{see} D_{tel}}$$

- As D increases, the resolving power decreases, unless W gets larger.

$$\theta_{see} = p \times \theta_{pix}$$

- p : the number of pixels across the slit image

$$R = \frac{(\sin i + \sin \theta)}{\cos i} \frac{D_{coll}}{D_{tel}} \frac{206265}{p \theta_{pix}}$$

## 5.2.2 Diffraction gratings

$$R = \frac{(\sin i + \sin \theta)}{\cos i} \frac{D_{coll}}{D_{tel}} \frac{206265}{p\theta_{pix}}$$

- the trade-offs of size( $p$ ) vs resolution ( $R$ )
- To maintain  $R$ , as the telescope diameter increases, the spectrograph gets larger ( $D_{coll}$  gets larger).

## 5.2.2 Diffraction gratings

- The intensity distribution ( $I$ ) from an ideal grating can be derived by expanding the analysis of wave interference from single and double slits to  $N$  slits (Chapter.2)

$$I = A_0^2 \frac{\sin^2 \beta}{\beta^2} \frac{\sin^2 N\gamma}{\sin^2 \gamma}$$

- $\gamma = \pi d \sin \theta / \lambda$  : the phase difference between adjacent of slits of separation  $d$ 
  - contribution of  $N$  slits
- $\beta = \pi b \sin \theta / \lambda$  : the phase difference from the center of on slit (width :  $b$ ) to its edge
  - represents the case of single slit

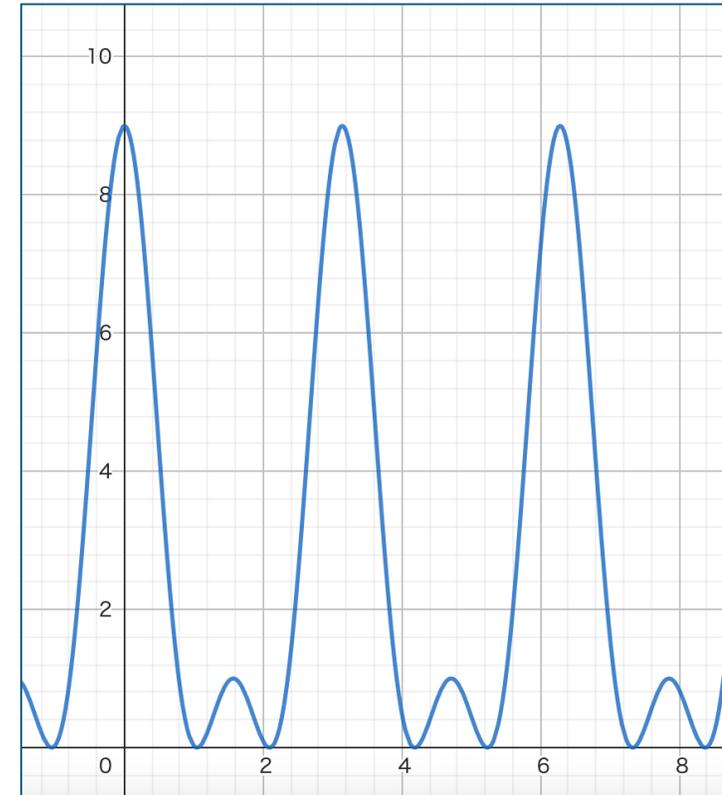
# 5.2.2 Diffraction gratings

$$I = A_0^2 \frac{\sin^2 \beta}{\beta^2} \frac{\sin^2 N\gamma}{\sin^2 \gamma}$$

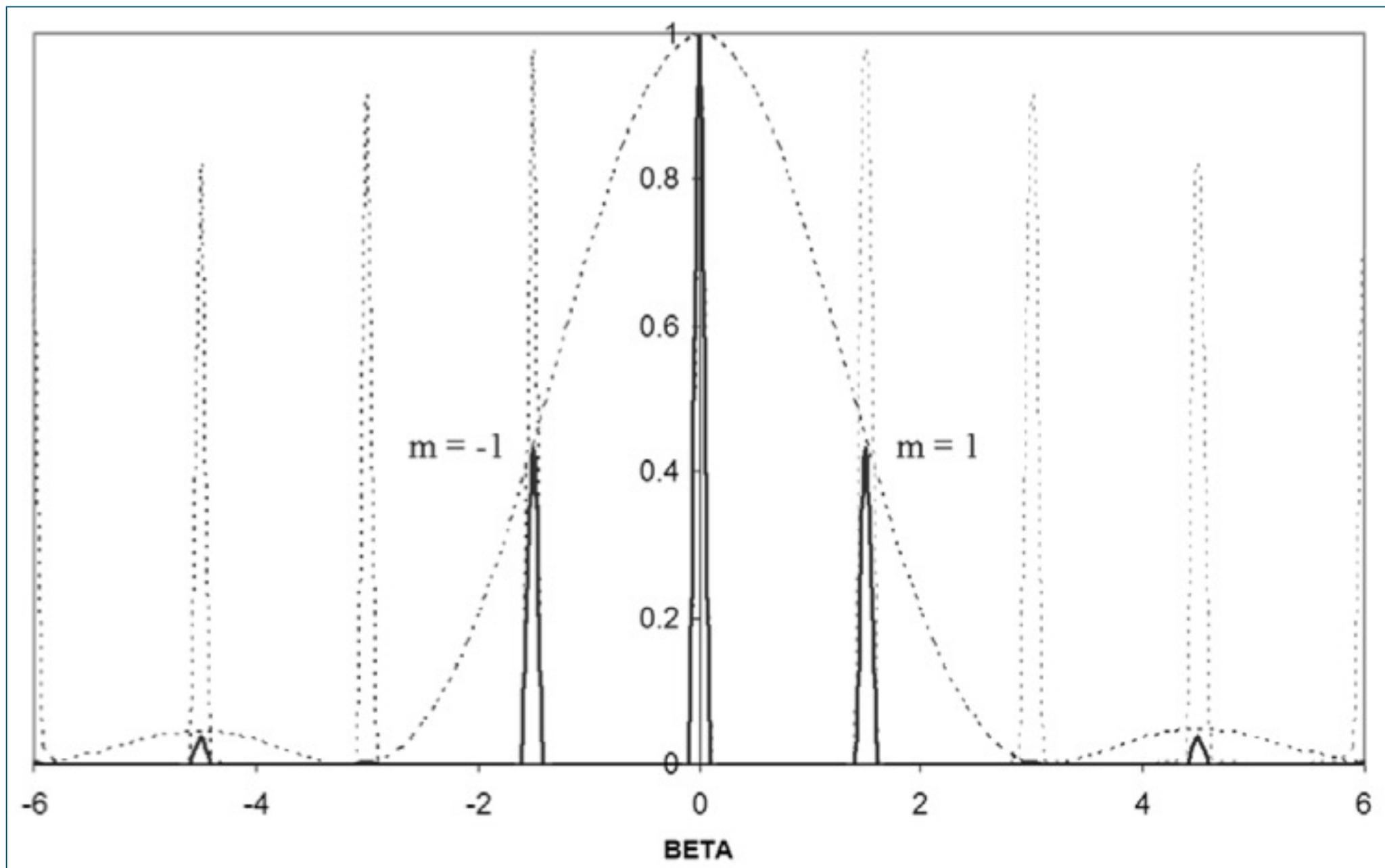
- $\frac{\sin^2 N\gamma}{\sin^2 \gamma}$  ( $\gamma = \pi d \sin \theta / \lambda$ )
  - strong maximum values equal to  $N^2$
  - $\gamma = 0, \pi, 2\pi \dots > d \sin \theta = m\lambda$
  - Secondary maxima between orders are strongly suppressed.
- $\frac{\sin^2 \beta}{\beta^2}$  ( $\beta = \pi b \sin \theta / \lambda$ )
  - first minimum value (0) when  $b \sin \theta = \lambda$

**Drastically reducing the intensity at  $m = \pm 1$**

$$y = \frac{\sin^2 3x}{\sin^2 x}$$



(produced by GeoGebra)

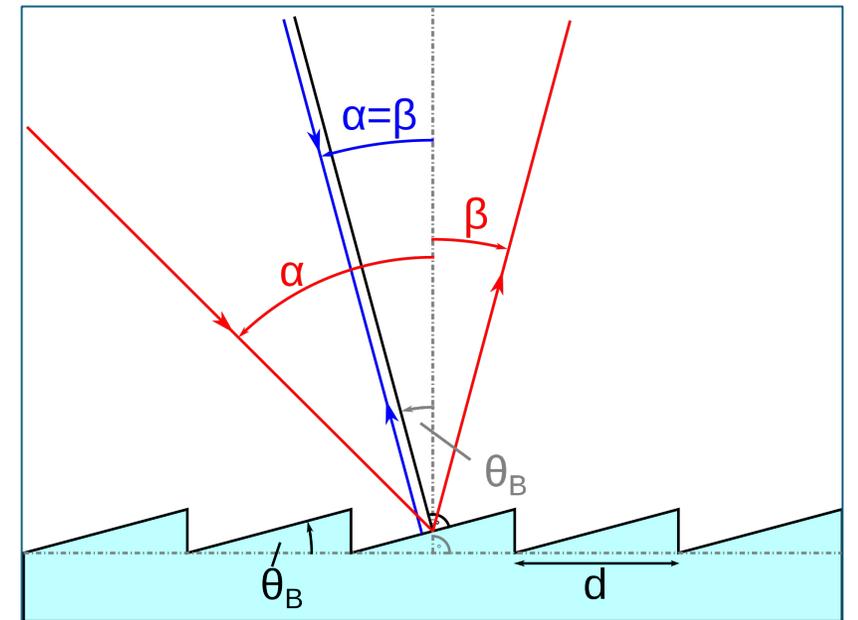


## 5.2.2 Diffraction gratings

- For any given order of diffraction, except  $m = 0$ , different wavelengths are diffracted **at different angles**.
  - > producing a spectrum
- when the single-slit diffraction pattern maximizes the diffracted intensity at zero order.
  - > no dispersion occurs. first/second order spectra are very faint.
- We need to be able **to “shift”** the peak of this envelope to  $m = 1$ .
- This is possible for reflection gratings.

## 5.2.2 Diffraction gratings

- by tilting the facets of a reflection grating through an angle  $\theta_B$  (**Blaze angle**) with respect to the plane of the grating surface,
  - it is possible to maximize the grating efficiency in the direction in which light would have been reflected in the absence of diffraction.
- $i(\alpha) + \theta(\beta) = 2\theta_B$  (most efficient)
- $i(\alpha) - \theta(\beta) = \phi$  (definition of spectrograph angle)
- $m\lambda_B = 2d \sin \theta_B \cos(\phi/2)$



(<https://astro-dic.jp/blaze-angle/>)

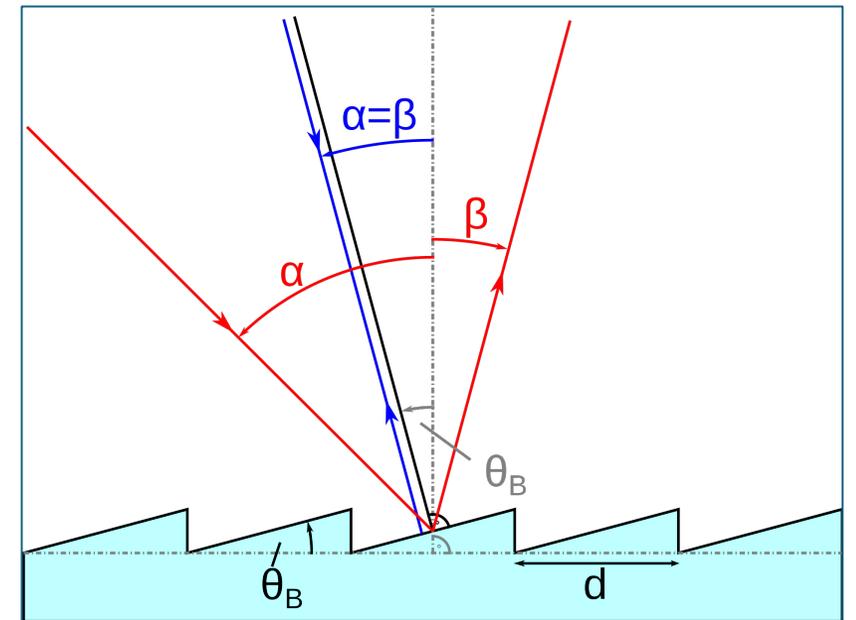
## 5.2.2 Diffraction gratings

$$m\lambda_B = 2d \sin \theta_B \cos(\phi/2)$$

- **“Littrow” condition**

- $\phi = 0$
- $i = -\theta = \theta_B$  the incident and diffracted angles measured relative to the grating normal are equal to each other

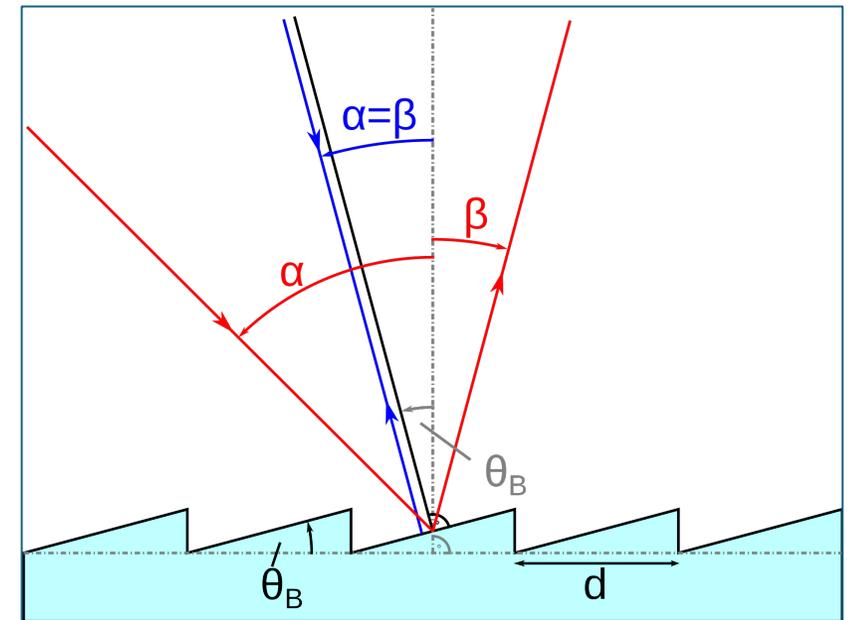
$$m\lambda_B = 2d \sin \theta_B$$
$$R = \frac{2D_{coll} \tan \theta_B}{p\theta_{pix}D_{tel}}$$



(<https://ja.wikipedia.org/wiki/ブレード回折角>)

## 5.2.2 Diffraction gratings

- The only way to work in the Littrow condition is with a central obscuration in the optics.
- Alternatively, one can use the “near” Littrow condition by moving off by  $10^\circ$  -  $20^\circ$  or the “**quasi**” Littrow condition by going out of the plane ( $\gamma > 0^\circ$ ).
  - Grating efficiency drops **rapidly** as the angle away from Littrow grows.
  - the drop is very **slow** for quasi-Littrow mode.
    - the slit image is tilted.



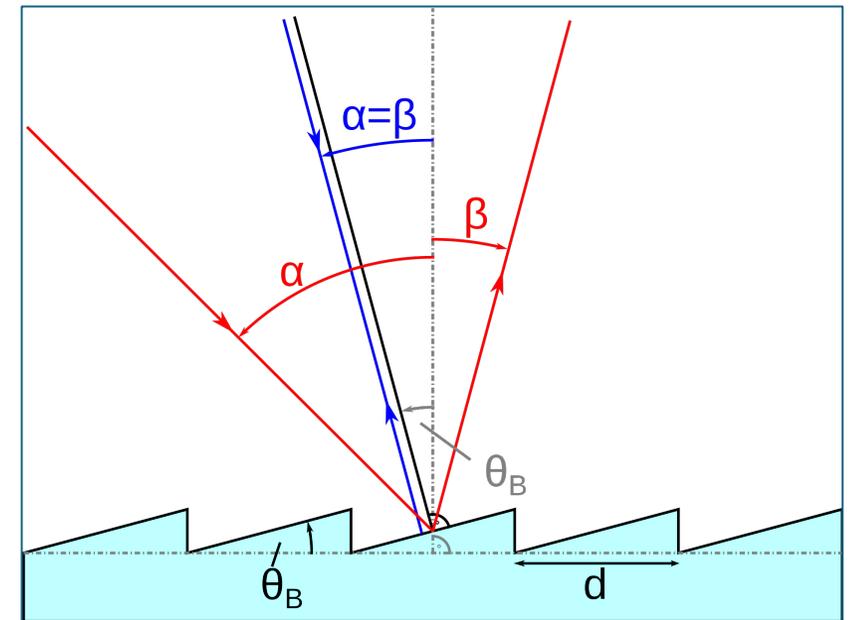
(<https://ja.wikipedia.org/wiki/ブレード回折角>)

## 5.2.2 Diffraction gratings

- the tilted angle  $\chi$

$$\tan \chi = \frac{\tan \gamma (\sin i + \sin \theta)}{\cos \theta}$$

- when  $\tan \theta_B = 2$  echelle grating,  $\tan \chi = 4 \tan \gamma$ 
  - $\gamma = 5^\circ > \chi = 19.3^\circ$
- there is also a change  $\Delta\chi$  in this angle across an order
  - the higher the order, the smaller the change



(<https://ja.wikipedia.org/wiki/ブレード回折角>)

## 5.2.2 Diffraction gratings

- for a given pair of incident and diffraction angles the grating equation is satisfied for all  $\lambda$  for which  $\mathbf{m}$  is an integer.

- There are two wavelengths in successive orders

$$m \lambda' = (m + 1)\lambda$$

- the wavelength difference  $\lambda' - \lambda$  is called Free Spectral Range (**FSR**)

$$\Delta\lambda_{FSP} = \lambda/m$$

- The two wavelengths are diffracted in the same direction
  - requires either an “order sorter” filter or a cross-disperser element(when  $m$  is large)
  - order sorting filters must be carefully chosen to cut on and off sharply to prevent order overlap (Section 5.4.3)

## 5.2.2 Diffraction gratings

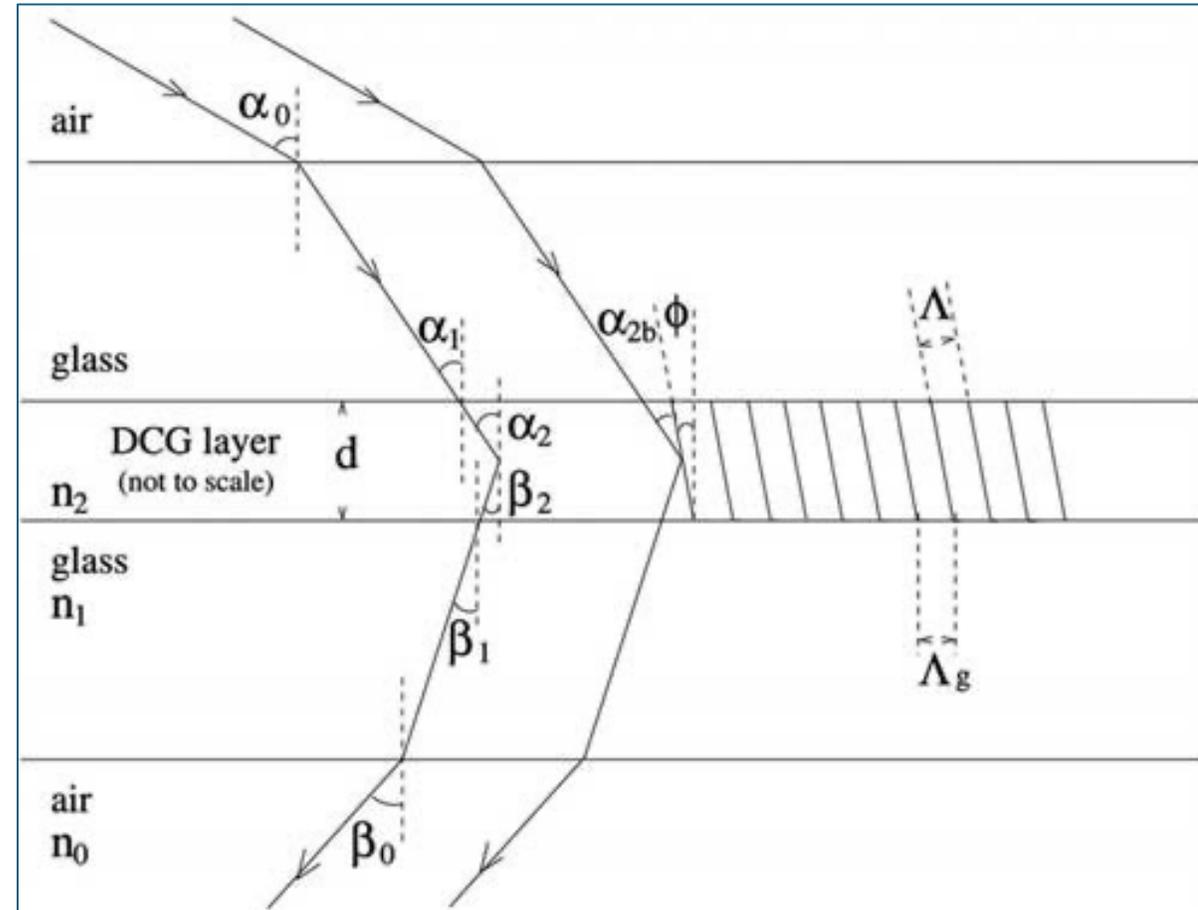
- Grating efficiency is difficult to calculate.
- Peak efficiency should occur at  $\lambda_B$  when  $m = 1$  and then declining peaks should occur at  $\lambda_B/m$  in subsequent orders.

## 5.2.2 Diffraction gratings

- Volume Phase Holographic (VPH) grating
  - a new technology for grating fabrication
  - an optical substrate in which the refractive index varies periodically throughout the body of the grating.
  - grating body is made from a thin(3-30 $\mu\text{m}$ ) slab of **dichromated gelatine(DCG)** trapped between glass plates

# 5.2.2 Diffraction gratings

- Light passing through a VPH transmission grating
$$m\lambda = n_i\Lambda_g(\sin \alpha_i + \sin \beta_i)$$
- $m$  : an integer of the order
- $n_i$  : the refractive index of the medium
- $\Lambda_g$  : the grating period (groove spacing)



# 5.2.2 Diffraction gratings

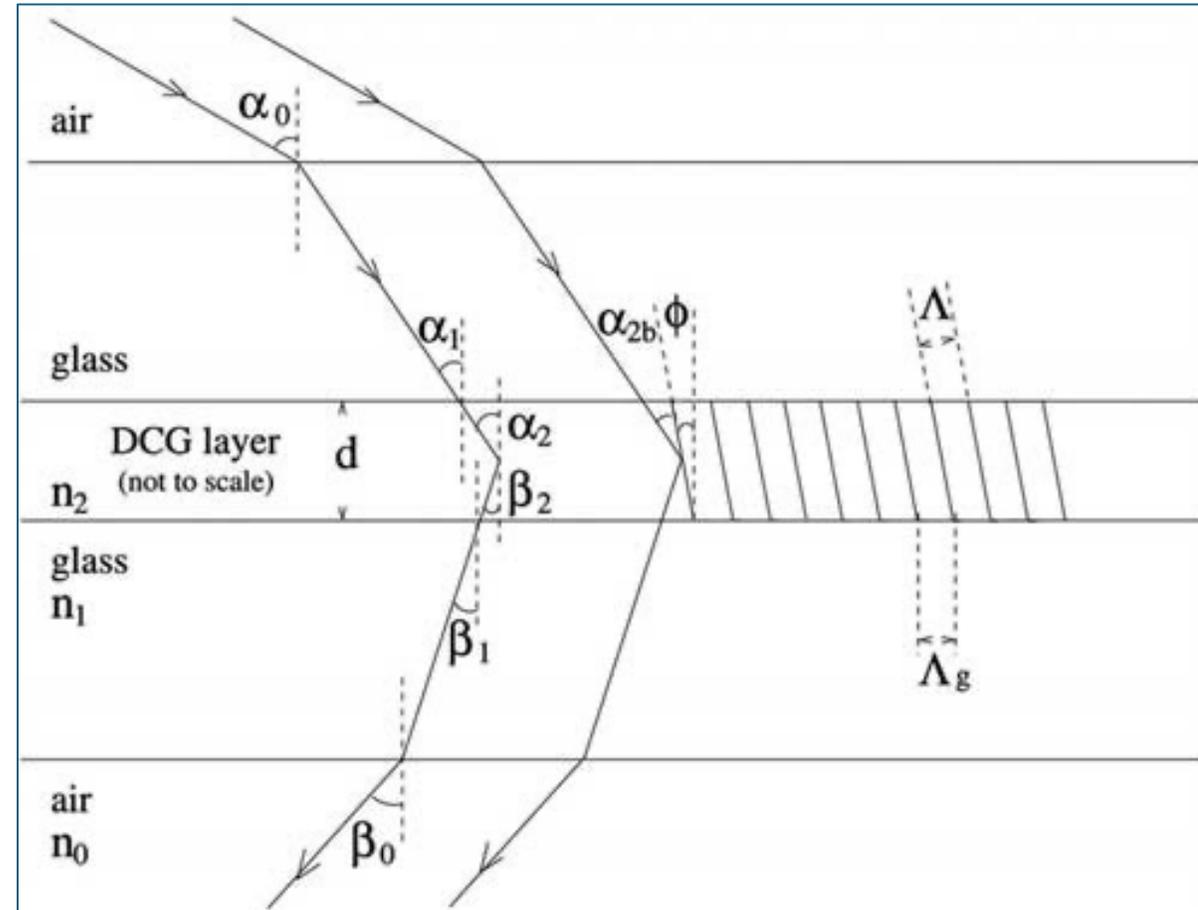
$$m\lambda = n_i \Lambda_g (\sin \alpha_i + \sin \beta_i)$$

- High diffraction efficiency can occur when light is effectively reflected from the plane of the fringes ( $\beta_2 + \phi = \alpha_2 - \phi$ ).

- the same as Bragg diffraction

$$m\lambda = 2n_2 \Lambda_g \sin \alpha_{2b}$$

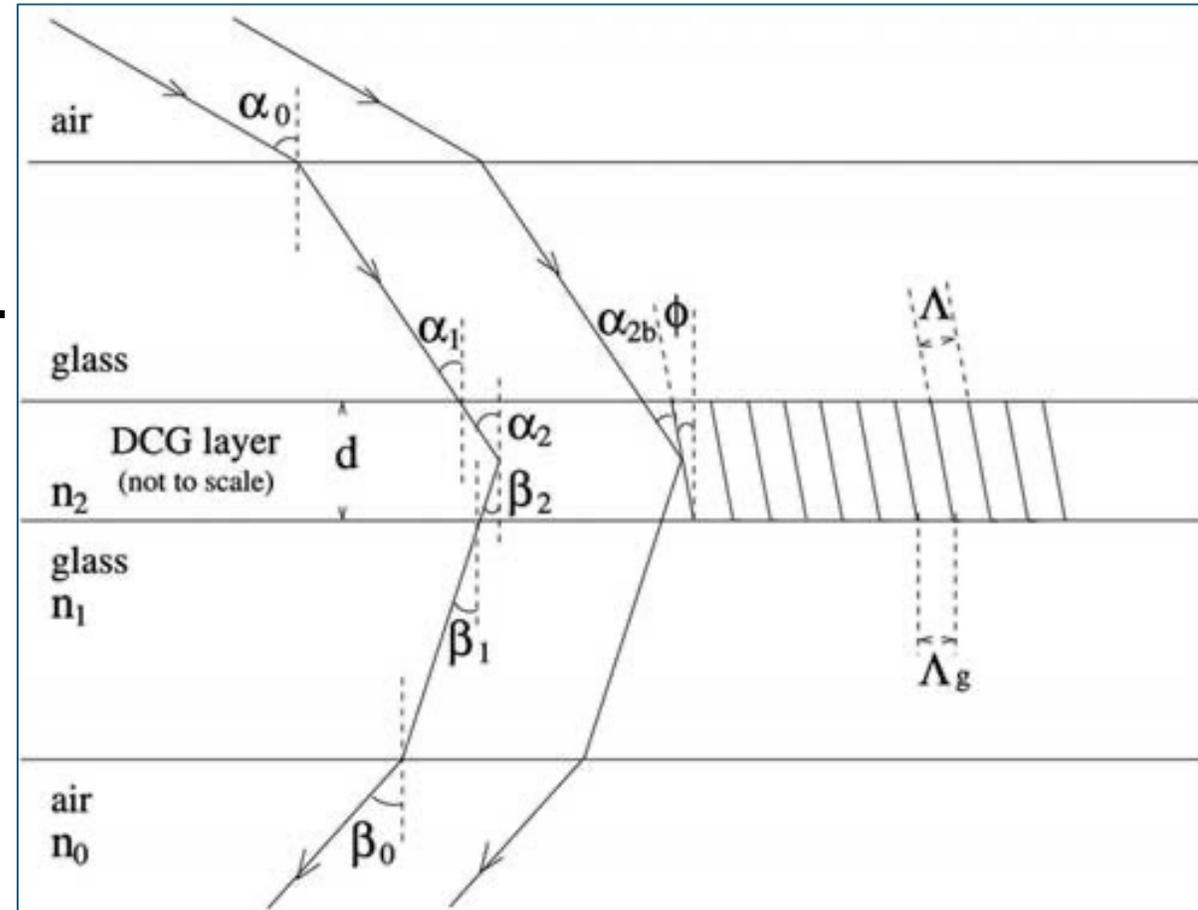
- $n_2$ : the refractive index of DCG layer
- $\alpha_{2b} = \alpha_2 - \phi$  : Bragg angle



## 5.2.2 Diffraction gratings

$$m\lambda = 2n_2\Lambda_g \sin \alpha_{2b}$$

- At wavelengths sufficiently displaced from the Bragg condition, there is no diffraction.
- Diffraction efficiency depends on the semi-amplitude of the refractive index modulation ( $\Delta n_2$ ) and the grating thickness ( $d$ ).

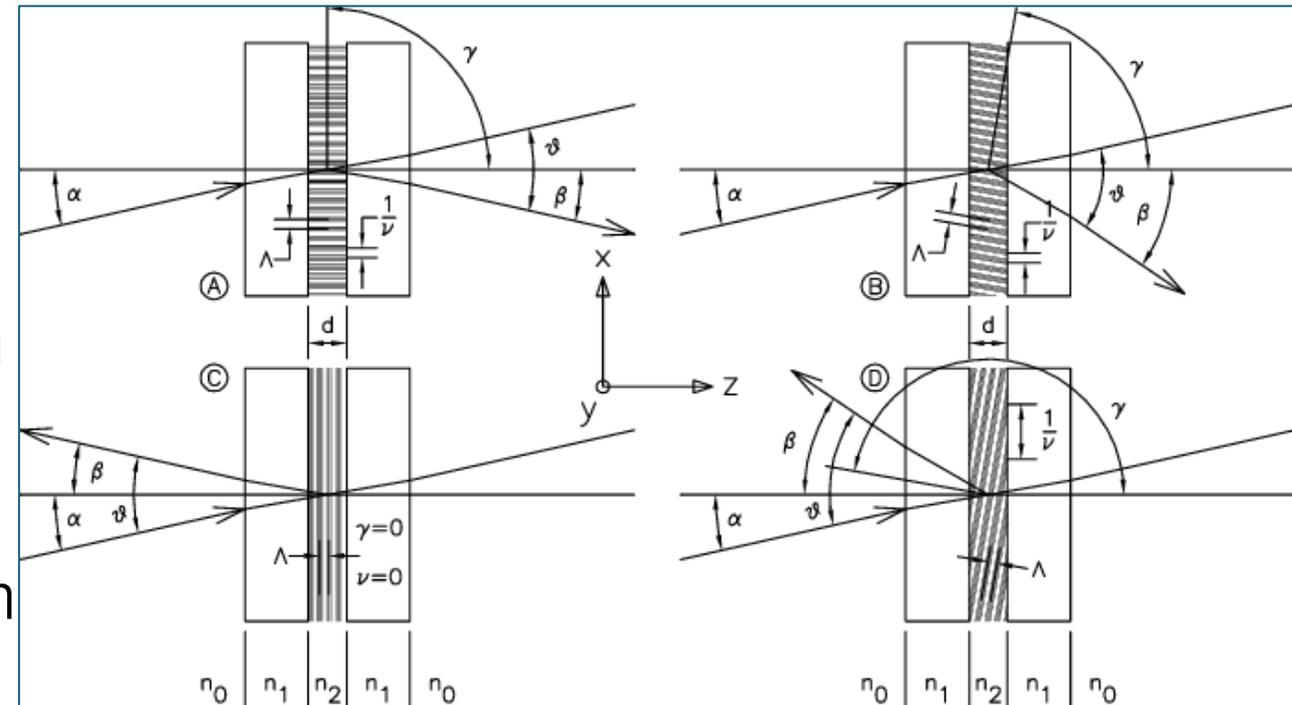




# 5.2.2 Diffraction gratings

$$m\lambda = 2n_2\Lambda_g \sin \alpha_{2b}$$

- One form for the refractive index  $n_2(x, z)$   
 $= n_2 + \Delta n_2 \cos[2\pi\nu_g(x \sin \gamma + z \cos \gamma)]$
- gives the variation in the x, z plane where z is the optical axis through the VPH, and  $\gamma$  is the angle between the normal to the planes and the z-axis.
- $\nu_g$  : line densities 300-6000lines/mm
- $\Delta n_2$ : 0.02-0.1



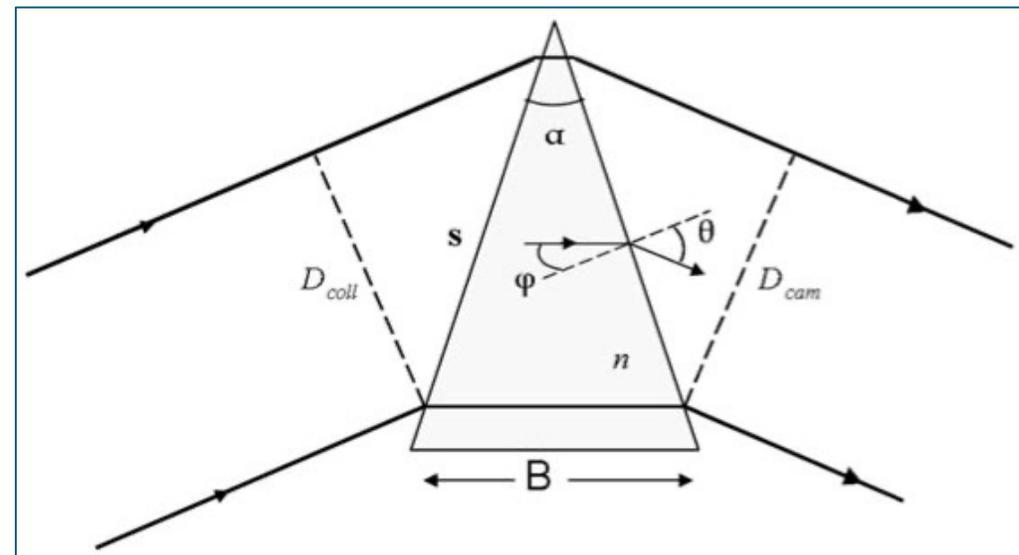
(Tunable Gratings: Imaging the Universe in 3-D with Volume-Phase Holographic Gratings Barden et al. 1999)

## 5.2.2 Diffraction gratings

- Because of Bragg condition, it is necessary to **articulate the camera to a new angle** to tune to a new wavelength.
- This area of technology is receiving a great deal of research attention, in part because of the possibility of making VPH gratings **in large sizes**.
- A VPH is used in the 6dF (six degree Field) spectrograph
- The use of “immersion” gratings
  - in which the grating surface is coupled to or embedded in a prism
  - so that  $n$  is returned to the grating equation  $m\lambda = 2dn \sin \theta$

# 5.2.3 Prisms

- Prism is used
  - as a primary disperser in (usually) low-resolution instruments
  - as a cross-disperser in high-resolution echelle spectrographs
- cheaper and easier to make
- no interference effects and no overlapping orders to handle
- × high resolving power is very difficult



# 5.2.3 Prisms

- Angular dispersion

$$\frac{d\theta}{d\lambda} = \frac{d\theta}{dn} \frac{dn}{d\lambda} = \frac{B}{D_{cam}} \frac{dn}{d\lambda}$$

- $\frac{dn}{d\lambda}$

- the wavelength dependency of the refractive index

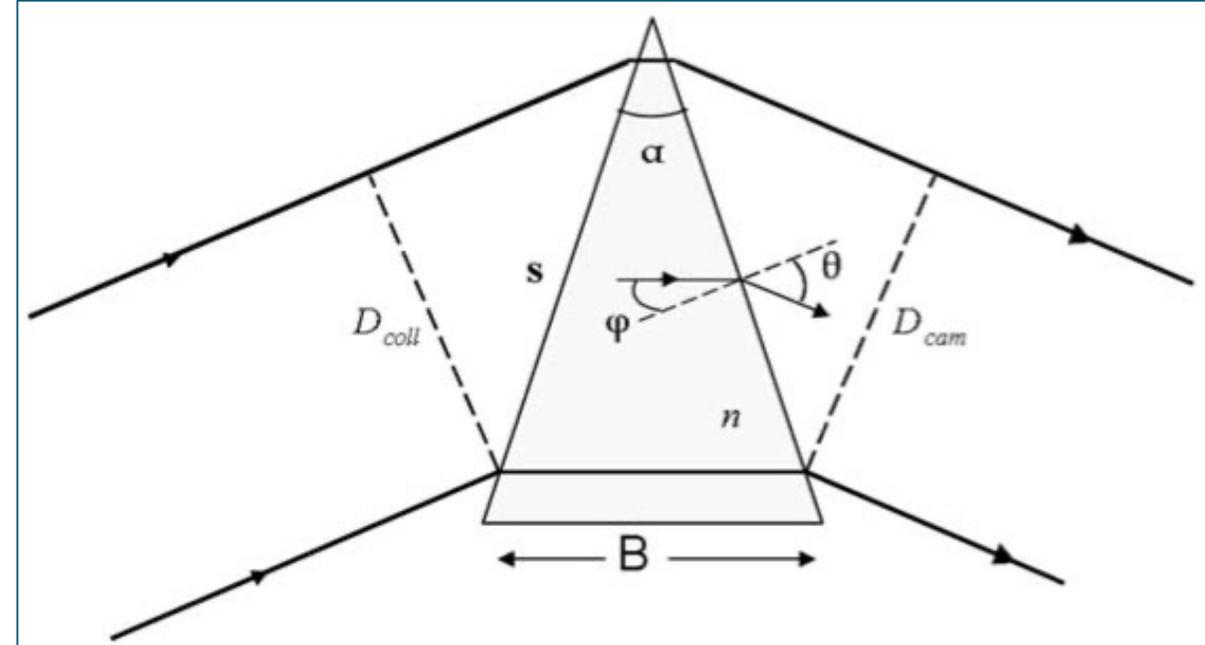
- $\frac{d\theta}{dn}$

- derived by differentiating Snell's law

- $\frac{d\theta}{dn} = [2s \sin\left(\frac{\alpha}{2}\right) / s \cos\theta]$

- $2s \sin\frac{\alpha}{2} = B$

- $s \cos\theta = D_{cam}$



## 5.2.3 Prisms

- Angular dispersion

$$\frac{d\theta}{d\lambda} = \frac{d\theta}{dn} \frac{dn}{d\lambda} = \frac{B}{D_{cam}} \frac{dn}{d\lambda}$$

- The resolving power of a prism

$$R = B \left( \frac{dn}{d\lambda} \right) \quad [D_{cam} d\theta = \lambda]$$

- for a slit-limited instrument

$$R = \frac{\lambda}{\theta_{res} D_{tel}} B \frac{dn}{d\lambda}$$

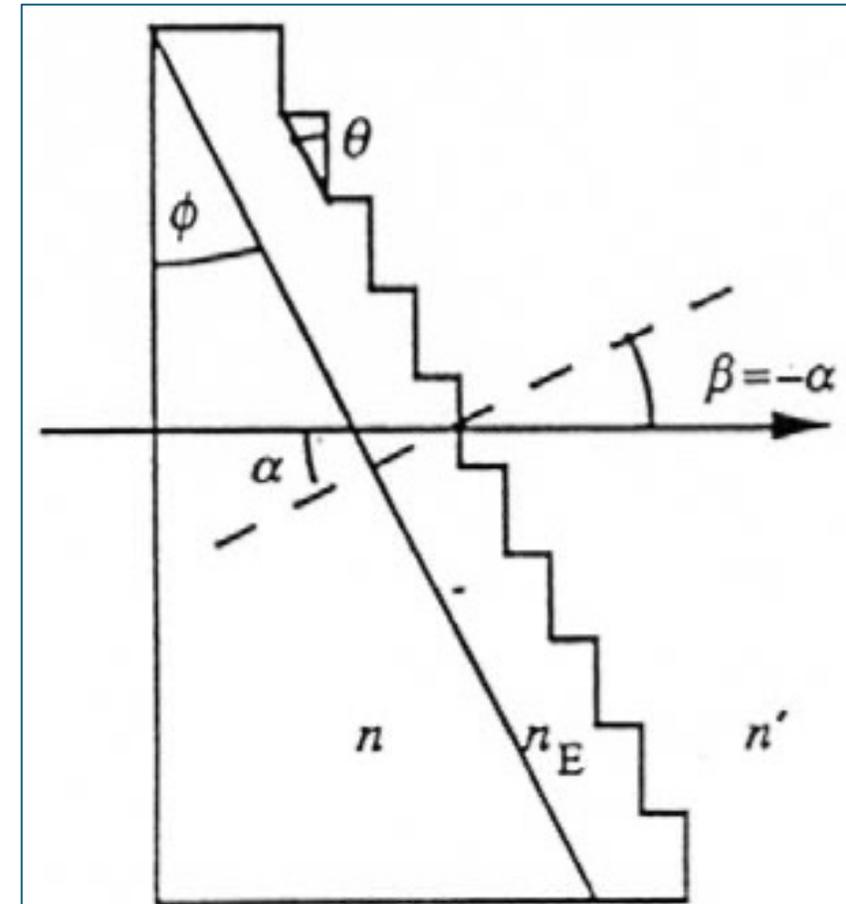
- $n$  usually increases steeply toward shorter wavelengths.
- the blue end of a prism is more spread out than the red end.

# 5.2.4 Grisms

- Grisms
  - hypotenuse(直角三角形の斜辺) > deviation of the prism
  - to bring the first order of diffraction on axis
- it can be placed in a filter wheel and treated like another filter.

$$m\lambda_c T = (n - 1) \sin \phi$$
$$R = \frac{EFL}{2d_{pix}} (n - 1) \tan \phi$$

- $T = 1/d$
- $\lambda_c$  : central wavelength
- EFL : the effective focal length of the camera system
- $R \sim 500-2000$



# Reference

[https://science.uct.ac.za/sites/default/files/content\\_migration/science\\_uct\\_ac\\_za/1471/files/spec1.pdf](https://science.uct.ac.za/sites/default/files/content_migration/science_uct_ac_za/1471/files/spec1.pdf)

<https://spectroscopy.wordpress.com/2020/05/12/basics-on-prisms-and-diffraction-gratings-part-1/>