3.Telescope

- the first element of any astronomical imaging system
- the means by which the light from distant objects is collected and focused
- good tracking, minimum air turbulence in the telescope dome
 →provide excellent telescope optics & good images
- consider basic optical properties and their applications to telescope design

- $\boldsymbol{\cdot}$ the end of 13C : convex lenses
- \cdot the middle of the 15C : concave lenses
- \cdot the beginning of the 17C : combination of convex & concave lenses
 - + 1608 : Hans Lippershey made a device with a convex & concave lens (3 \times)
 - + 1609 : Galileo Galilei made the telescope (8 \times , 20 \times)
 - \cdot small field of view of about 15 arcmin (only a quarter of the full moon)
 - \cdot produced an upright image
 - 1.52-1.83m in length
- \cdot the middle of 17C: length of astronomical telescope of 4.57-6.10m
 - \cdot 1656, Christiaan Huygens made the telescope
 - 7 meters long
 - 10cm aperture of objective lens
 - \cdot magnification 100 \times
 - field of view of 17 arcmin

- a spherical-shaped lens : rays parallel to the optical axis fail to converge at one point
 - =spherical aberration
 - \cdot to eliminate spherical aberration
 - →lens curvature : plane & hyperbolic or spherical & elliptical
- Curved lens : the colors decomposed from white light come to a focus at a different point on the optical axis

=chromatic aberration

⇒cause the image of a star to be surrounded by circles of different colors

to reduce spherical & chromatic aberration
 →telescopes with long focal length

- 1672 : Isaac Newton had constructed the first reflecting telescope using a spherical mirror
 - $\boldsymbol{\cdot}$ used a 2-inch mirror blank of speculum metal
 - \cdot placed the mirror at the bottom of a tube
 - \rightarrow caught the reflected rays on a secondary mirror at 45° near the top of the tube \rightarrow secondary mirror reflected the image into a convex lens outside the tube
- others were unable to grind mirrors of regular curvature & the mirror tarnished easily
 ⇒ reflecting telescope remained a curiosity for decades
- around 1723 : John Hadley had perfected better polishing techniques
 →the first parabolic version of the Newtonian telescope was

 \rightarrow the first parabolic version of the Newtonian telescope was made

- the middle of 18C : many reflecting telescopes with primary mirrors up to 6-inch in diameter had been produced
- the latter half of the 18C : large reflecting telescope with parabolic ground mirrors came into their own
 - William Herschel built a reflector with a mirror diameter 1.22m and a 12.2m focal length
 - to tackle the problem of rapid tarnishing in metal mirrors, Herschel always had a spare ready to exchange
 - \rightarrow remained the largest telescope for over 50 years

- classical times : the size of a telescope was characterized by its focal length modern telescopes : identified by diameter of the primary aperture or by the diameter of the equivalent circle with the same collecting surface area
- The largest telescope used by Galileo : diameter of 4.4cm
 2008 : 10 general-purpose optical telescopes with effective diameters >8m

 \cdot the doubling time for aperture size was about 50 years up until about 1950

 \cdot after 1950, the telescopes have been doubling in size



Figure 3.1. The growth of aperture size with time is plotted from the invention of the telescope to present day. Credit: René Racine.

 1993, the largest telescope (Keck telescope) went into operation the first of a pair of 10m telescopes employed the "segmented mirror" (The second telescope was inaugurated in May 1996)

• many telescopes with collecting apertures >6.5m in diameter, and employing different technologies, were under construction or being contemplated

- \cdot the introduction and growth of CCDs
 - \rightarrow more and more area on the sky could be digitally imaged to deeper levels
- the use of multi-slit devices and optical fibers to observe many objects simultaneously
 →the efficiency of spectroscopy had been improved

• to construct larger ground-based telescopes and to develop methods for counteracting the image-blurring effects of air turbulence

 \rightarrow gain large factors in efficiency

fundamental issues

(1) how to achieve a very large collecting aperture of the required optical performance

(2) how to support and control in the optimum way such a very heavy mechanical structure

(3) how to enclose a very large telescope in a cost-effective way with negligible degradation on image quality due to vibration, air disturbance, or inadequate environmental protection (wind, dust).

- new telescopes
 - must be designed to capitalize on the best seeing conditions
 - must be designed with remote control in mind
 - must give sharper images than their predecessors
 - \rightarrow it all comes down to how the mirrors are made and supported

segmented mirrors

• smaller monolithic disks of thin polished glass

• Each segment is individually supported and global changes are sensed at the gaps between segments.

meniscus mirrors

• large monolithic disks of solid glass which are so thin that it must be accepted that they will be flexible

• must be actively controlled to maintain the required shape during operation

honeycomb mirrors

• thick mirrors are constructed but large pockets of mass are removed to make the mirror lightweight yet very stiff

Table 3.2.	The current	generation	of telescopes	with	$D > 6.5 {\rm m}.$
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Telescope and date	Primary (m)	Mirror technology	Location			
Keck I, II (1993, 1996) (CARA)	10	Hexagonal segments of Zerodur	Mauna Kea, Hawaii			
Hobby–Eberly Telescope (2000)	9.2	Hexagonal segments Spherical primary				
South African Large Telescope (2004)	9.2	Hexagonal segments Spherical primary	Sutherland, SA			
LBT (2005, 2008) (former Columbus)	2 × 8.4	Borosilicate honeycomb	Mt. Graham, Arizona			
Subaru (2000) (Japan)	8.2	Thin meniscus	Mauna Kea, Hawaii			
VLT1, 2, 3, 4 (1998, 2000, 2001, 2002) (ESO)	4 × 8.2	Thin meniscus	Cerro Paranal, Chile			
Gemini N, S (2000, 2002) (GTP)	2 × 8.0	Thin meniscus	Mauna Kea, Hawaii Cerro Pachón, Chile			
Magellan I, II (2002, 2003) (OCIW)	6.5	Borosilicate honeycomb	Las Campanas, Chile			
MMT upgrade (2002) (SI/UA)	6.5	Borosilicate honeycomb	Mt. Hopkins, Arizona			

- Larger and faster primary mirrors require new polishing methods.
 - \cdot the problem is the asphericity
- →difference of curvature from place to place and between tangential and radial directions
- A rigid pitch lap can't accommodate the changes of curvature of a strongly aspheric surface
- To polish the primary mirror blank for the 4.2m Herschel Telescope
 →used lap which changed shape as it moved (stressed lap polishing)
 - The method was based on the fact that, when a full-sized lap is used to make polishing strokes across a paraboloid, the distortion required to maintain contact is that of coma.

3.2 Telescope designs

- Three basic types of telescopes
 - refractive: dioptric, using lenses
 - reflective: catoptric, using mirrors
 - hybrid: catadioptric, using a combination of lenses and mirrors
- hybrid designs are most popular for amateur astronomy
- all large professional telescopes are reflectors



 $\cdot\,$ when a ray of light strikes the boundary between two different transparent materials, it is divided into a reflected ray and a refracted ray

• A ray represents the direction of flow of the energy in an electromagnetic wave and is perpendicular to the wavefront.

- \cdot the law of reflection : $\theta = \varphi$
- the law of refraction : $n\sin\theta = n'\sin\theta'$
- the refractive index : $n = \frac{c}{v} = \sqrt{\varepsilon_r \mu_r} (\varepsilon_r$:relative permittivity, μ_r :relative permeability)
- The distance between crests inside the material is now λ/n .
- · dispersion: the angular divergence of light of different wavelengths

dispersive power= $\frac{1}{v} = (n_F - n_C)/(n_D - 1)$ (F:486nm(blue), D:589nm(yellow), C:656nm(red))

• optical path=nd (n:refractive index, d:distance that light travels)

• Fermat's principle : the path taken by a light ray in going from one point to another through any set of media is such as to render its optical path equal, in the first approximation, to other paths closely adjacent to the actual one.

- paraxial optics : approximation in which angles are sufficiently small $\rightarrow \sin\theta = \theta$ to first order
 - $\theta = 10^{\circ} \rightarrow \text{Error} \approx 0.5\%$ $\theta = 30^{\circ} \rightarrow \text{Error} < 5\%$
 - \cdot systems with large focal ratios (f/D) meet the paraxial approximation.

- the thin lens equation in air or vacuum : $\frac{1}{f} = \frac{1}{s} + \frac{1}{s'}$, $m = -\frac{s'}{s} = \frac{h'}{h}$, $f/number = \frac{f}{D}$ (f:the focal length, s,s':the object & image disatance, h,h':the object & image heights, m:the lateral or transverse magnification, D:the clear aperture diameter of the lens)
- the spherical mirror equation : $\frac{1}{f} = \frac{1}{s} + \frac{1}{s'} = \frac{2}{R}$, $m = -\frac{s'}{s} = \frac{h'}{h}$ (R:the radius of curvature of the mirror)
- optical power and the lensmaker's formula : $P = \frac{1}{f} = (n-1)\left[\frac{1}{R_1} \frac{1}{R_2} + \frac{t(n-1)}{nR_1R_2}\right]$ (P:the power of the lens(diopter[1/m]), R_1, R_2 :the radius of curvature of the front & back surface, t:the central thickness of the lens)
 - thick lenses or two thin lenses separated by a distance d

$$\Rightarrow P = P_1 + P_2 - \left(\frac{n}{d}\right)P_1P_2$$





図2.正レンズで実像が作られる場合のレンズの公式の導出(1)



図2.レンズメーカーの公式(単レンズの焦点距離)の導出

• Newton's equation : $x'x = f^2$

(x=s-f, x'=s'-f)

most useful for calculating the amount of re-focus required

- angular magnification : $M = \frac{\tan u'}{\tan u} = \frac{s}{s'} = \frac{h}{h'}$ (u,u':the angle of incident & refracted ray respect to the optical axis) defined in terms of the slope angles of the rays
- the lagrange invariant : *nhtanu = n'h'tanu'* (n,n':the refractive indices in object and image space)
 The quantity (*nhtanu*) is constant in a system with refracting or reflective surfaces.

Kepler's telescope

 \cdot If the eyepiece is moved along the axis such that the real image formed by the objective lens coincides with the focal point of the eyepiece , then the emergent rays are parallel and the final image is at infinity

 \cdot the telescope is afocal and the image is inverted.

- · Galileo's telescope
 - the eyepiece lens : concave
 - the lenses are separated by the difference of their focal lengths
 - the system is afocal but the image in a Galilean telescope is upright →more convenient for terrestrial use.



Fig. 1.1. (a) Galileo telescope and (b) Kepler telescope.



Figure 3.3. The principle of the astronomical telescope. The objective lens and the eyepiece lens are represented by vertical lines with double-ended arrows.

• The objective lens defines the aperture or "stop" and it is said to form the "entrance pupil" for the system.

 \rightarrow the objective lens itself is a relatively nearby object for the eyepiece lens and an image of the entrance pupil is formed behind lens E (the "exit" pupil)

· chief ray: passed through the center of both the entrance and exit pupils.

- the magnifying power: $M = \theta'/\theta$
- $h = s \tan \theta = s' \tan \theta'$, $s = f_o + f_e$, $f_e = -s' \Rightarrow M = -f_o/f_e$
- $M = D_o/D_e$

 $(D_o, D_e:$ the diameter of the objective lens & the exit pupil)

 \cdot the advent of CCD imaging

 \rightarrow most astronomical telescopes do not employ an eyepiece, but form images directly onto the detector pixels in the telescope's focal plane.

Iongitudinal chromatic aberration

The horizontal distance along the optical axis between the different focal positions

lateral chromatic aberration

The vertical difference in image height

 $\cdot\,$ the classical method for correcting chromatic aberration is to use two lenses of different materials in contact to make an achromatic doublet

 $\Rightarrow P_D = P'_D + P''_D = (n'_D - 1)K' + (n''_D - 1)K''$ (D:yellow line of Na, the prime: the crown glass, the double prime: the flint glass, $K = \frac{1}{R_1} - \frac{1}{R_2}$) $P_F = P_C \Rightarrow \frac{K'}{K''} = -\frac{n''_F - n''_C}{n'_F - n'_C}$ the negative sign out front implies that one lens must be concave $\frac{P'_D}{P''_D} = -\frac{V'}{V''}$ these are the dispersion constants for the two glasses $P'_D = P_D[V'/(V' - V'')], P''_D = -P_D[V''/(V' - V'')]$

• select the required focal length $f_D(=1/P_D)$

 \cdot select the best pair of glasses from the glass table on the basis of their dispersion constants $V' {\rm and} \, V''$

- $\boldsymbol{\cdot}$ calculate the powers of each lens
- derive K' and K'' where P'_D and P''_D are defined
- $\boldsymbol{\cdot}$ find the radii from the definition of K

• To facilitate cementing of the convex and concave lenses, the second radius of the first lens should match the first radius of the second lens

 $\rightarrow {R^{\prime\prime}}_1 = {R^\prime}_2$

· it is convenient to use the same radius on the entrance face of the convex lens

$$\rightarrow R'_2 = -R'_1$$

• R''_2 : adjusted to give the required power P''_D

• Keeping the more curved crown glass element towards the incoming light reduces spherical aberration

• Colors outside the corrected range can still cause a halo of color around a point source, referred to as the ``secondary'' spectrum.

 $\cdot\,$ the sheer size and weight of large achromatic doublets reaching 1 m in diameter

 \rightarrow switched to mirrors



・光学技術の基礎用語

<u>https://www.optics-words.com/kikakogaku/thin-lens-</u> <u>equation.html</u>

• Jingquan Cheng, "The Principals of Astronomical Telescope Design", Springer